REPRINTED FROM CHEMISTRY AND INDUSTRY, 1966, pp. 239-240

A New Synthesis of Sulphonylureas by Carbonation of Sulphonamides under Pressure

By B. R. Franko-Filipasic and R. Patarcity

High Pressure Laboratory, Central Research Department, FMC Corporation, Princeton, New Jersey, U.S.A.

We report a new synthesis of symmetrical bis(sulphonyl)ureas, (RSO₂NH)₂CO, by pressure carbonation of the sulphonamide in the presence of potassium carbonate (equation (i)). Although the potassium salt of the sulphonamide can be carbonated

 $2RSO_2NH_2 + 2CO_2 + 2K_2CO_3 \rightarrow$

 $RSO_2NKCONHSO_2R+3KHCO_3$... (i) directly (equation (ii)), the first procedure is not only $2RSO_2NHK + 2CO_2 \rightarrow$

 $RSO_2NKCONHSO_2R+KHCO_3 \dots \dots$ (ii) more convenient, avoiding the preparation of the hygroscopic salt, but also gives higher yields. As the bis(sulphonyl)ureas are sufficiently acidic to react with carbonate or bicarbonate in the cold, the monopotassium salt is isolated from the reaction.

Symmetrical bis(sulphonyl)ureas are difficult to synthesise and are rarely encountered in the literature. carbon dioxide under pressure for 3-12 hours. The reaction products are rock hard and must be chipped from the autoclave. The solids are ground, suspended in water, and the insoluble sulphonamide is removed by filtration. The filtrate is titrated (pH meter) with cold dilute hydrochloric acid: any soluble potassium sulphonamide reacts with acid at a pH above 7 and the sulphonamide is removed by filtration. The bis(sulphonyl)ureas precipitate in a pH range of 4.3 to 2.7; acidification is continued to 0.5 and stirring continued for 30 minutes to completely free the urea of salt.

Potassium carbonate was the only alkali or alkaline earth carbonate to participate in the reaction; m-nitrophenyl- and 2,5-dichlorophenyl sulphonamides failed to react. No side reactions or ring carbonation were observed under these reaction conditions.

Table Bis(sulphonyl)ureas by pressure carbonation (RSO₂NH)₂CO

		Reaction					
		Nitrogen (%)			Time	Temp.	CO_2
R	<i>m.p.</i> (°C)	Found	Theory	Yield	(hr)	(°C)	(psig)†
C_6H_5	154-5	8.18	8.23	55	3	165	4000
p-CH ₃ C ₆ H ₄	99-101d*	7.18	7.25	85*	3	165	4000
o-CH ₃ C ₆ H ₄	111-112	7.92	7.61	77	3	165	4000
p-ClC ₆ H ₄	134-136*	6.46	6.56	54*	12	165	4000
p-ClC ₆ H ₄	170-171	7.06	6.85	76	12	165	3900
3,4-Cl ₂ C ₆ H ₃	138-144	5.48	5.64	88	12	200	3700
n-C4H9	119-120	9.59	9.32	35	12	150	4000

* Monohydrate.

† Pressure at maximum temperature.

The attempted coupling of the sulphonamide with phosgene¹ usually results in sulphonylisocyanate, RSO₂NCO² the reaction of the sulphonylisocyanate with sulphonamide has been utilised.³ Treatment of the sodium salt of sulphonamide with phosgene4 and treatment of urea with sulphonyl chloride⁵ are generally unsuccessful. The reaction of phenyl carbonate with the sodium⁶ or potassium⁷ salt of the sulphonamide is the only useful method.

Yields of 35-85% (see Table) can be obtained in a pressure autoclave by treating one mole of sulphonamide and two moles of potassium carbonate with

The bis(sulphonyl)ureas exhibit a characteristic carbonyl absorption band in the region of 1700-1750 cm⁻¹.

Received December 3, 1965

References ¹ Tischendorf, J., *J. prakt. Chem.*, 1895, **51**, [2] 350 ² British Patent 692,360 (1950)

³ Billeter, O. C., Ber. dt. chem. Ges., 1904, 37, 695

⁴ East Ger. Patent 4255 (1940)

⁵ Kurzer, F., Chem. Rev., 1952, **50**, 13 ⁶ Field, L. & Grunwald, F. A., J. Am. chem. Soc., 1953, **75**,

⁹³⁴ ⁷ Burmistrov, S. I. & Dubina, V. L., Chem. Abs., 1963, **59**,

High pressure research in metals

by B. R. Franko-Filipasic and W. J. McCarthy

The High Pressure Laboratory, Chemical Research & Development Centre, FMC Corporation, P.O. Box 8, Princeton, New Jersey, 08540, USA

Progress in high pressure chemical research has been limited by the inability to operate completely in the metal of choice: all reactor assemblies contain at least two different metal surfaces exposed to the reagents, a fact which the experimenter often does not realise. The common assemblies (Fig. 1) used in research consist of a body (A) and head (B) of



Fig. 1 Reactor schematic (A) body; (B) head; (C) heater-shaker; (D) pressure gauge; (E) gauge isolators; (F) rupture assembly; (G) valve; (H) tubing coil; (I) cap

the same metal housed in an electric heater-shaker unit (C); the pressure gauge (D) and possibly a gauge isolator (E); rupture assembly (F); valves (G); and tubing (H) connected to the gas supply – a flexible connexion, allowing the assembly to shake, is provided by coiling the tubing.

Extraneous metals open to the reagents are found in:

1. *Head and thermowell gaskets*. These gaskets are usually of stainless steel, copper or silver.

2. *Valve closure*. The valve body and stem are usually a type of stainless steel; some other metals are available.

3. *Tubing*. The reactor is connected to valving with stainless steel tubing; very few alternatives are available that are sufficiently flexible and can contain the pressure.

4. *Rupture assembly*. The housing and discs are usually stainless steel, but discs of various metals are available in limited bursting ranges.

5. *Pressure gauge*. The gauge is usually of a Bourdon type of various alloy steels; gauge isolators are stainless steel.

Scrupulous catalytic research under these conditions is a very real problem, especially since the stainless steels in the assembly also vary.

The authors' system has been redesigned to make possible operation in the metal of choice with 'Teflon' as the only extraneous material, by reducing the system to a reactor and a multipurpose valve closure (Fig. 2).

1. The reactor closure has been redesigned to confine a glassfilled 'Teflon' (15/85) gasket (a) in such a way that operations to 400°c and 10,000 psig have been achieved. The gasket is 0.031in thick and 0.25in wide; the clearance between the head ridge and the body groove is 0.005 in. The gasket flows out slightly during operation and must be

replaced after every run. The thermowell gasket (b) is of the same material.

2. A new valve closure has been designed and tested incorporating a rupture assembly (c) and a gauge isolator (d) with a 'Teflon' piston (e). In many reactions where it is not necessary to have a pressure gauge on the reactor, a similar valve without a gauge isolator is used. All process wetted portions of the valve, stem, gauge isolator and rupture assembly are of the metal of choice and 'Teflon'.



Fig. 2 Multipurpose valve in reactor head (a) head gasket; (b) thermowell gasket; (c) rupture assembly; (d) gauge isolator; (e) 'Teflon' piston; (f) gas connexion; (g) rupture disc

3. No tubing is open to the process, as the valve closure is seated directly in the head. The gas connexion (f) is above the valve stem seat 90° from the rupture assembly.

4. Although rupture discs are available in various metals, the simplest solution is to cover a metallic rupture disc (g) with a 3mm sheet of 'Teflon'. Only under extreme temperature conditions does this fail.

5. The gauge isolator is connected to either a standard gauge or a pressure sensor.

With this system it has been possible to operate in any one type of stainless steel, titanium, aluminium, nickel, Carpenter 20 and various alloys. This equipment was designed and manufactured to the authors' specifications by Pressure Products Industries, Hatboro, Pennsylvania, 19040.

> Received 17 August 1970 Revised 23 September 1970

APR 201971

Printed by Richard Madley Ltd., 54 Grafton Way, London, WIP 5LB England